

# Analysis of Longitudinal Leaky SAW on Quartz Thin Plate Bonded to Similar-material Substrate

水晶同種接合構造上の縦型漏洩弾性表面波の解析

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## 1. Introduction

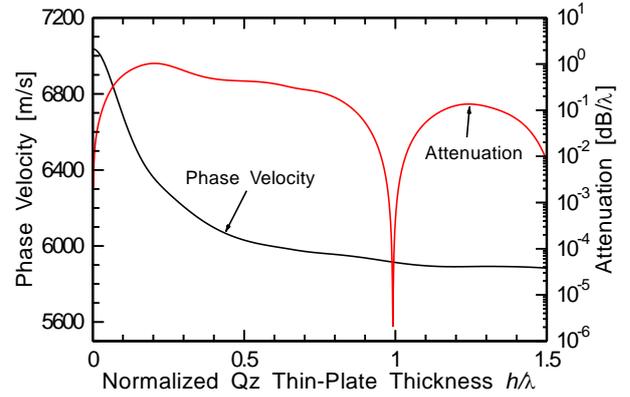
High-performance surface acoustic wave (SAW) devices with characteristics such as high frequency, large bandwidth (BW), and high  $Q$  factor are required for next-generation communication systems. In our laboratory, we clarified theoretically that better resonance properties can be obtained for a leaky SAW (LSAW) on a similar-material bonded structure of Quartz (Qz) with different cut angles.<sup>1</sup>

In this study, the propagation and resonance properties of a longitudinal LSAW (LLSAW) with high phase velocity on a bonded structure comprising a Qz thin plate and a Qz support substrate are investigated theoretically.

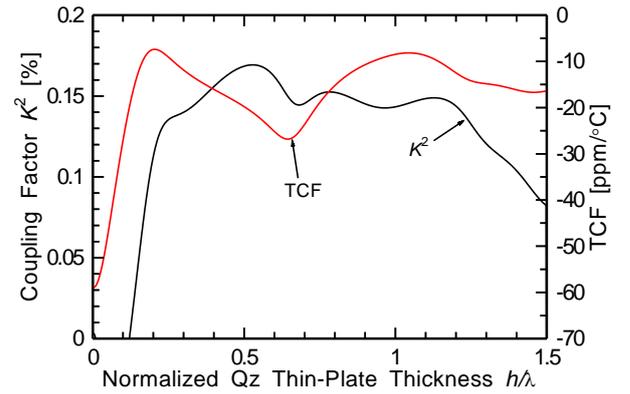
## 2. Calculation of Propagation Properties

The propagation properties (phase velocity, attenuation, coupling factor ( $K^2$ ), and temperature coefficient of frequency (TCF)) for the thin-plate thickness  $h/\lambda$  normalized by wavelength  $\lambda$  on a bonded structure using an X-cut Qz (X-Qz) as the thin plate were calculated. First, X41°Y-Qz was chosen as a support substrate because it has the highest phase velocity in the X-Qz (Euler angle:  $(90^\circ, 90^\circ, \psi)$ ) for LLSAW. When a thin plate was chosen to be X176.5°Y-Qz, a small attenuation was obtained at a certain thin-plate thickness. **Figure 1** shows the propagation properties of LLSAW on the X176.5°Y-Qz/X41°Y-Qz. The attenuation shows a minimum value ( $1.8 \times 10^{-5}$  dB/ $\lambda$ ) at  $h/\lambda=0.99$ . The  $K^2$  at  $h/\lambda=0.99$  is 0.14%, which is about 50 times higher than the  $K^2$  (0.0026%) of the single X41°Y-Qz. Furthermore, the TCF of at  $h/\lambda=0.99$  is  $-8.6$  ppm/ $^\circ\text{C}$ , which is about sevenfold lower than the TCF ( $-58.9$  ppm/ $^\circ\text{C}$ ) of the single X41°Y-Qz.

Second, AT39°X-Qz with a high phase velocity for LLSAW was also chosen as a support substrate, and X160°Y-Qz as a thin plate was found to exhibit a small attenuation when combined with the support substrate. **Figure 2** shows the propagation properties of LLSAW on X160°Y-Qz/AT39°X-Qz. The attenuation is minimum value ( $6.7 \times 10^{-4}$  dB/ $\lambda$ ) at  $h/\lambda=0.18$ . The  $K^2$  at  $h/\lambda=0.18$  is 0.15%, which is about 330 times higher than the  $K^2$  (0.00046%) of the single



(a) Phase velocity and attenuation



(b)  $K^2$  and TCF

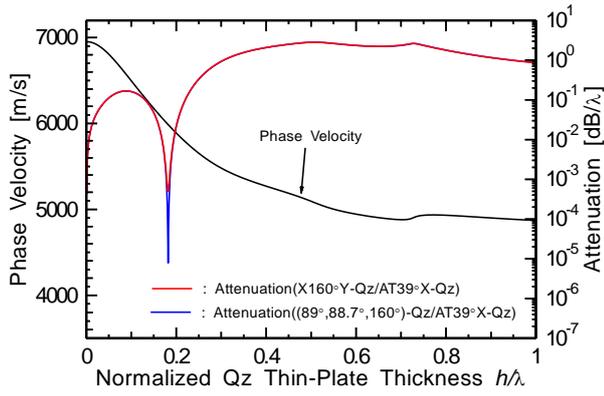
Fig. 1 Calculated propagation properties of LLSAW on X176.5°Y-Qz/X41°Y-Qz.

AT39°X-Qz. Furthermore, the TCF at  $h/\lambda=0.18$  is  $7.8$  ppm/ $^\circ\text{C}$ , which is about sixfold lower than the TCF ( $-42.4$  ppm/ $^\circ\text{C}$ ) of the single AT39°X-Qz. It was also found that zero TCF appeared at  $h/\lambda=0.16$ ,  $0.6$  and  $0.72$ .

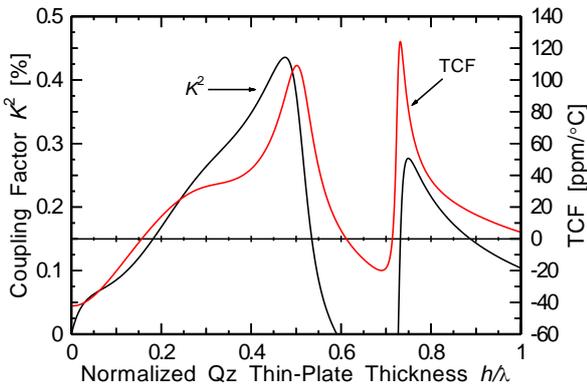
Moreover, the attenuation was reduced by optimizing the Euler angle of the thin plate. For the  $(89^\circ, 88.7^\circ, 160^\circ)$ -Qz/AT39°X-Qz bonded structure, a smaller attenuation ( $7.9 \times 10^{-6}$  dB/ $\lambda$ ) than that of X160°Y-Qz/AT39°X-Qz at  $h/\lambda=0.18$  was obtained, as shown in Fig. 2(a).

## 3. Simulation of Resonance Properties

By a finite element method, we analyzed the resonance properties of an LLSAW in the case of forming an infinitely periodic interdigital transducer (IDT) with a period  $\lambda$  of  $8.0 \mu\text{m}$  and an Al thin film ( $h_{\text{Al}}$ : thickness).



(a) Phase velocity and attenuation



(b)  $K^2$  and TCF

Fig. 2 Calculated propagation properties of LLSAW on X160°Y-Qz/AT39°X-Qz.

A perfect matching layer was provided at the bottom of the support substrate with a  $10\lambda$  thickness. The mechanical loss was not taken into consideration. The resonance properties of X176.5°Y-Qz/X41°Y-Qz ( $h/\lambda=0.98$ ,  $h_{Al}/\lambda=0.005$ ), (89°,88.7°,160°)-Qz/AT39°X-Qz ( $h/\lambda=0.18$ ,  $h_{Al}/\lambda=0.00125$ ), and a single X176.5°Y-Qz are shown **Fig. 3**. The  $h_{Al}$  values were optimized for each case so that a larger admittance ratio is obtained. In Fig. 3, the horizontal axis is converted from the frequency  $f$  to the phase velocity  $v$  using the relationship  $v=f\lambda$ .

As shown in Fig. 3 and **Table I**, a high admittance ratio and high resonance and antiresonance  $Q$  factors ( $Q_r$ ,  $Q_a$ ) can be obtained at a phase velocity of approximately 6,000 m/s by utilizing bonded structures, whereas the single Qz has a slight resonance for LLSAW.

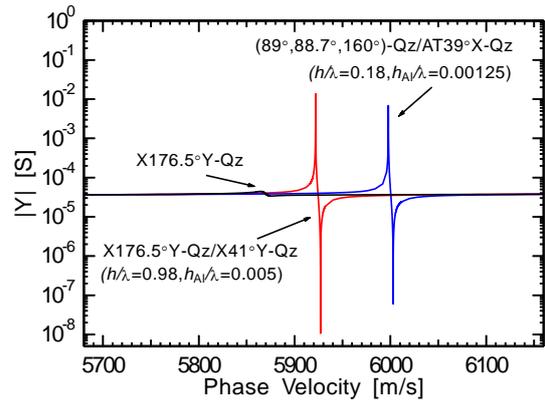


Fig. 3 Simulated resonance properties of LLSAW on single Qz substrate, X176.5°Y-Qz/X41°Y-Qz, and (89°,88.7°,160°)-Qz/AT39°X-Qz.

The X59°Y-Qz( $h/\lambda=0.40$ )/X41°Y-Qz was also found to have a large resonance property. The X176.5°Y-Qz/X41°Y-Qz exhibits the largest resonance property with the admittance ratio of 122 dB among these bonded structures. The (89°,88.7°,160°)-Qz/AT39°X-Qz shows 26 dB larger admittance ratio (101 dB), 2.3 times higher  $Q_r$  (107,100), and eight times higher  $Q_a$  (375,200) than those for the X160°Y-Qz/AT39°X-Qz.

The fractional BWs of these structures ranged from 0.070 to 0.086%. The construction of a filter with a large BW and steep cutoff characteristics can be expected by combining the bonded structure with a ceramic LC filter having broad cutoff characteristics.

#### 4. Conclusions

In this study, the propagation and resonance properties of LLSAW on a bonded structure comprising a Qz thin plate and a Qz support substrate were investigated theoretically. It was found that LLSAWs with low attenuation and large admittance ratio, which cannot be achieved with a single Qz, appear when an X-Qz thin plate is bonded to an X-Qz support substrate with a different propagation direction. As the next step, we will investigate such bonded structures experimentally.

#### References

1. T. Fujimaki, *et al.*, JJAP **60** (2021) SDDC04.

Table I Simulated resonance properties.

	Admittance ratio [dB]	Fractional BW [%]	$Q_r$	$Q_a$
X59°Y-Qz( $h/\lambda=0.40$ )/X41°Y-Qz	78	0.082	216,700	288,980
X176.5°Y-Qz( $h/\lambda=0.98$ )/X41°Y-Qz	122	0.086	185,060	740,880
X160°Y-Qz( $h/\lambda=0.18$ )/AT39°X-Qz	75	0.070	46,900	46,900
(89°,88.7°,160°)-Qz( $h/\lambda=0.18$ )/AT39°X-Qz	101	0.083	107,100	375,200