## Mechanical Q factor dependence on Zr / Ti ratio of sputter-grown PZT epitaxial thin films

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#### 1. Introduction

 $Pb(Zr_xTi_{1-x})O_3$  (PZT) bulk ceramics are widely used for ultrasonic transducers and actuators because of their high piezoelectricity. On the other hand, PZT single crystalline thin films are attractive for GHz band thin-film resonator applications because of their expected higher mechanical Q factor (Q<sub>m</sub>) than polycrystalline films. However, there are few reports on the Q<sub>m</sub> of PZT single crystal thin film resonators.

Our group previously proposed a method to evaluate  $Q_m$  of the piezoelectric film without removing the substrate.<sup>1</sup> This method can determine  $Q_m$  of piezoelectric thin films grown on the substrates with a difficulty of etching, such as SrTiO<sub>3</sub>.

In this study,  $Q_m$  of sputter-grown PZT epitaxial films grown on La-SrTiO<sub>3</sub> substrates was measured by using this method. The dependence of  $Q_m$  of Pb(Zr<sub>x</sub>Ti<sub>1-x</sub>)O<sub>3</sub> films on Zr / Ti ratio was investigated.

# 2. Principle of evaluating Q<sub>m</sub> of the thin film with HBAR structure

 $Q_m$  of the entire HBAR ( $Q_{entire}$ ) is affected by two factors:  $Q_m$  of the substrate ( $Q_{sub}$ ) and  $Q_m$  of the thin film ( $Q_{piezo}$ ). Since the mass of the film layer is much smaller than the mass of the substrate in the typical HBAR,  $Q_{entire}$  is nearly equal to the  $Q_{sub}$ . Nevertheless,  $Q_{piezo}$  has a more significant influence on  $Q_{entire}$  especially near the thickness resonant frequency of the thin film.

When  $Q_{piezo}$  is lower than  $Q_{sub}$ , the acoustic damping of the piezoelectric thin film results in the decrease of overall  $Q_{entire}$  in the vicinity of the resonant frequency of the thin films. The decrease in  $Q_{entire}$  near the resonant frequency of the thin film is determined by the ratio of  $Q_{sub}$  to  $Q_{piezo}$ . Therefore,  $Q_{piezo}$  can be estimated by using  $Q_{sub}$  as a reference.

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#### 3. Extraction of mechanical Q factor of PZT

Epitaxial (001) Pb( $Zr_xTi_{1-x}$ )O<sub>3</sub> films with different Zr / Ti ratio (*x*=0, 0.2, 0.4, 0.5, 0.6) were grown on conductive (100) La-SrTiO<sub>3</sub> single crystal substrate by RF magnetron sputtering. Ten mol% PbO rich PZT powder sputtering target is used to maintain the stoichiometry of PZT films.<sup>2</sup>

The real part of impedance ( $Z_{real}$ ) was measured by a network analyzer (E5071C, Keysight Technologies) with various top electrode areas.  $Q_{entire}$ was acquired from multiple resonance peaks in the  $Z_{real}$ .  $Q_{piezo}$  was extracted by fitting the theoretical  $Q_{entire}$  to the experimental  $Q_{entire}$  in the vicinity of the resonant frequency of the films. Theoretical  $Q_{entire}$ was simulated by using Mason's equivalent circuit model.

**Figure 1** shows the typical  $Q_{entire}$  of  $Pb(Zr_xTi_{1-x})O_3 / La-SrTiO_3$  HBAR structure when x = 0. In this case,  $Q_m$  of the PbTiO\_3 films was estimated to be 380.



Fig. 1  $Q_m$  factor of PbTiO<sub>3</sub> / La-SrTiO<sub>3</sub> HBAR structure and  $Q_m$  of PbTiO<sub>3</sub> thin film

#### 4. Results and discussions

The relationship between  $Q_m$  of Pb(Zr<sub>x</sub>Ti<sub>1-x</sub>)O<sub>3</sub> films and Zr concentration is shown in **Fig. 2**. In this  $Q_m$  measurement method, the evaluated  $Q_{piezo}$  has an electrode area dependence.<sup>3</sup> The electrode area dependence of  $Q_m$  of Pb(Zr<sub>x</sub>Ti<sub>1-x</sub>)O<sub>3</sub>, as shown in **Fig. 3**, should be caused by the leakage of acoustic waves in the lateral direction as surface acoustic waves. In this measurement, the highest value among

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the extracted  $Q_m$  is assumed to be the most accurate value owing to the minimum lateral acoustic wave leakage effect. As shown in Fig. 2,  $Q_m$  of Pb(Zr<sub>x</sub>Ti<sub>1-x</sub>)O<sub>3</sub> films decreases with increasing Zr concentration. Therefore, PbTiO<sub>3</sub> film is expected to possess the highest  $Q_m$ . In addition, we previously found that PbTiO<sub>3</sub> films exhibit the highest  $k_t^2$  for sputter-grown PZT epitaxial thin films.<sup>4</sup> the product of  $k_t^2$  and Q ( $k_t^2$ ·Q), known as the figure of merit (FoM) of BAW resonator, indicates that PbTiO<sub>3</sub> film is the most suitable for resonator applications among the PZT material (**Fig. 4**).

According to a previous report of our group, sputter-grown Pb( $Zr_xTi_{1-x}$ )O<sub>3</sub> thin films with all Zr concentrations show the tetragonal structure and do not have morphotropic phase boundary (MPB), which is identified around x = 0.53 in bulk PZT.<sup>4</sup> However, a characteristically high Q<sub>m</sub> of 400 was observed around MPB (x = 0.5).



Fig. 2 The relationship between  $Q_m$  of  $Pb(Zr_xTi_{1-x})O_3$  films and Zr concentration



Fig. 3 The relationship between  $Q_m$  of  $Pb(Zr_xTi_{1-x})O_3$  films and electrode area



Fig. 4  $k_t^2 \cdot Q$  and  $k_t^2$  of Pb(Zr<sub>x</sub>Ti<sub>1-x</sub>)O<sub>3</sub> films as a function of Zr concentration x

#### 5. Conclusion

 $Q_m$  of sputter-grown Pb( $Zr_xTi_{1-x}$ )O<sub>3</sub> epitaxial thin films were evaluated at various Zr concentration (x = 0, 0.2, 0.4, 0.5, 0.6). The results show that  $Q_m$  of Pb( $Zr_xTi_{1-x}$ )O<sub>3</sub> films decreases with increasing Zr concentration. When x = 0,  $Q_m$  of PbTiO<sub>3</sub> thin film exhibit 380, and  $k_t^2 \cdot Q$  exceeds 100. Therefore, PbTiO<sub>3</sub> epitaxial thin films are potential candidates for filter applications. On the other hand, a characteristically high  $Q_m$  of 400 was observed at x = 0.5, which is near the MPB of bulk PZT.

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#### References

- 1. S. Kinoshita and T. Yanagitani, Proc. IEEE Ultrason. Symp. 299 (2019).
- K. Iijima, Y. Tomita, R. Takayama, and I. Ueda, J. Appl. Phys. 60 (1) 361 (1986).
- 3. N. Iwata, S. Kinoshita, and T. Yanagitani, Proc. IEEE Ultrason. Symp. 2095 (2020).
- R. Noda, T. Shimidzu, K. Wasa, and T. Yanagitani, Proc. IEEE Ultrason. Symp. 13 (2019).